

# **Predictive Modeling of Tool Wear in Hard Turning**

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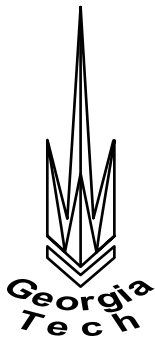
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# *Introduction and motivation*

- Hard turning process is defined as single point turning of materials harder than 50HRc and differs from conventional turning in:
  - Workpiece material property
  - Chip formation mechanism
  - Cutting tool required
  - Cutting condition applied
- It offers possible benefits over grinding process:
  - Lower equipment costs
  - Shorter setup time
  - Reduced process steps
  - High material removal rate
  - Better surface integrity
  - Elimination of cutting fluid

# Challenging issues in hard turning technology



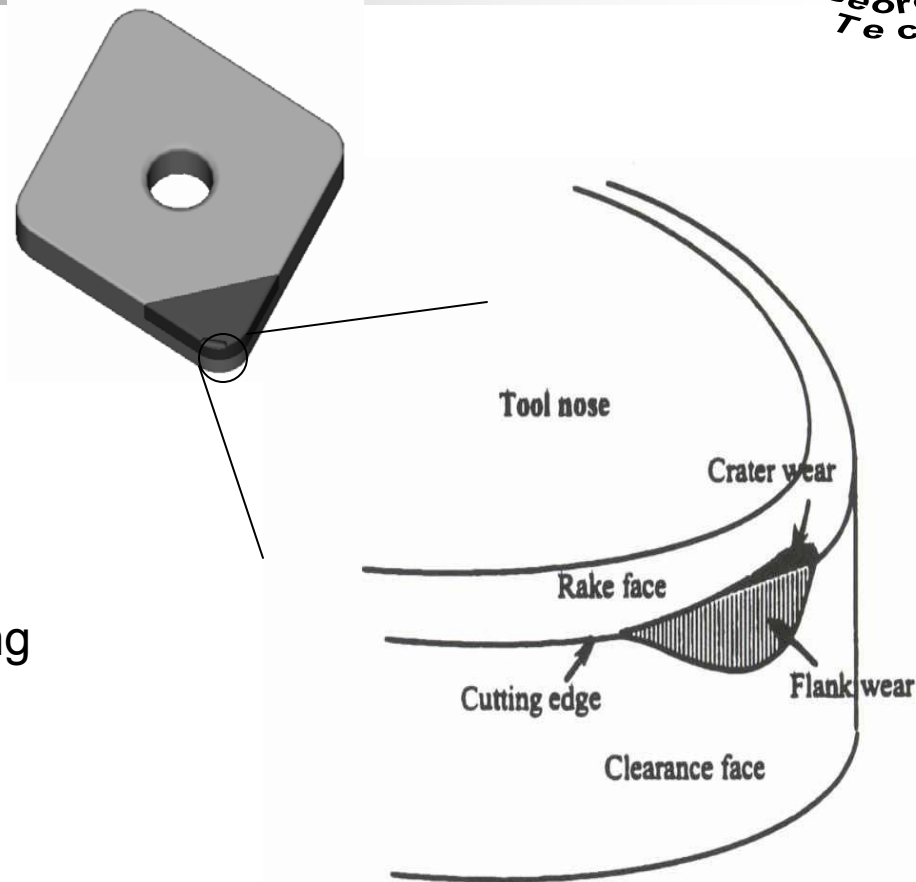
- The top issues to be solved in hard turning process:
  - **Tool wear** <Our researching interest>
    - Form accuracy
    - Surface integrity
    - Economic consideration
- Why tool wear:
  - High cost of CBN cutting tool, which is generally applied in hard turning
  - Cost of down-time for tool changing affects the economic justification of hard turning
- What to do about tool wear:
  - To find a relationship defining tool wear rate as the function of cutting condition and tool geometry for a given tool/work combination in hard turning

# *Factors influencing wear rate*

- Tool material's composition
  - CBN particle size and CBN content
  - Binder materials
  - Applied coating material and coating thickness
- Cutting condition
  - Feedrate
  - Depth of cut
  - Cutting speed
- Tool geometry
  - Rake angle for up-sharp tool
  - Chamfer length and angle, rake angle for chamfered tool
  - Hone radius, rake angle for honed tool
  - Tool nose radius

# Tool wear in hard turning

- Wear patterns in metal cutting
  - Crater wear
  - Flank wear
  - Depth of cut notching
  - Thermal shock crack
  - Nose wear
  - Chipping
  - Tool breakage
  - Built-up edge
- Wear mechanisms in metal cutting
  - Abrasion
  - Adhesion
  - Attrition
  - Fatigue
  - Dissolution/diffusion
  - Tribochemical process



Wear pattern in metal cutting

A decorative graphic consisting of overlapping yellow, red, and blue squares with a black crosshair.

## ***Tool wear in hard turning (cont'd)***

### Main wear patterns in hard turning

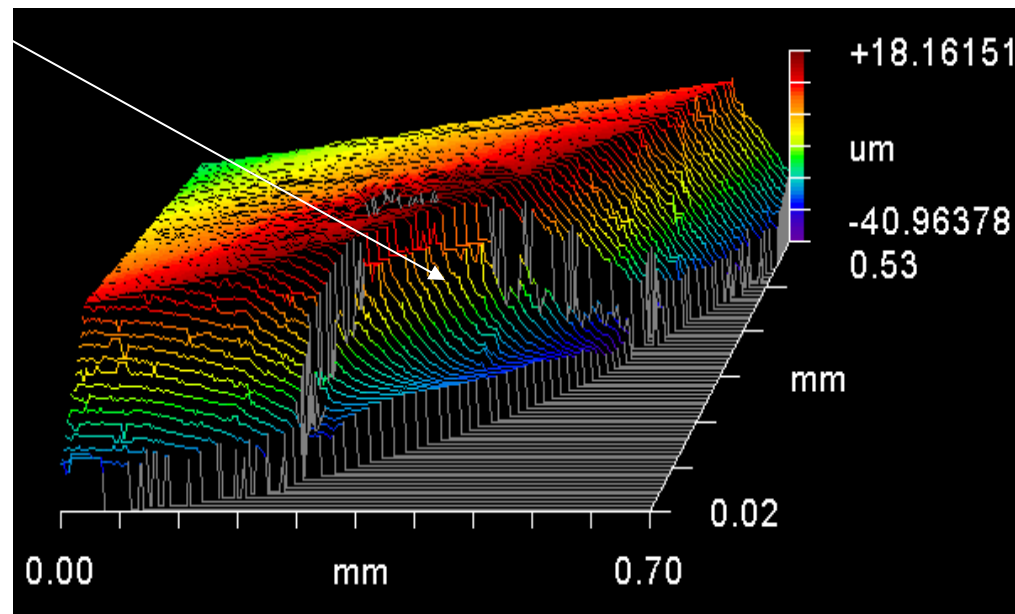
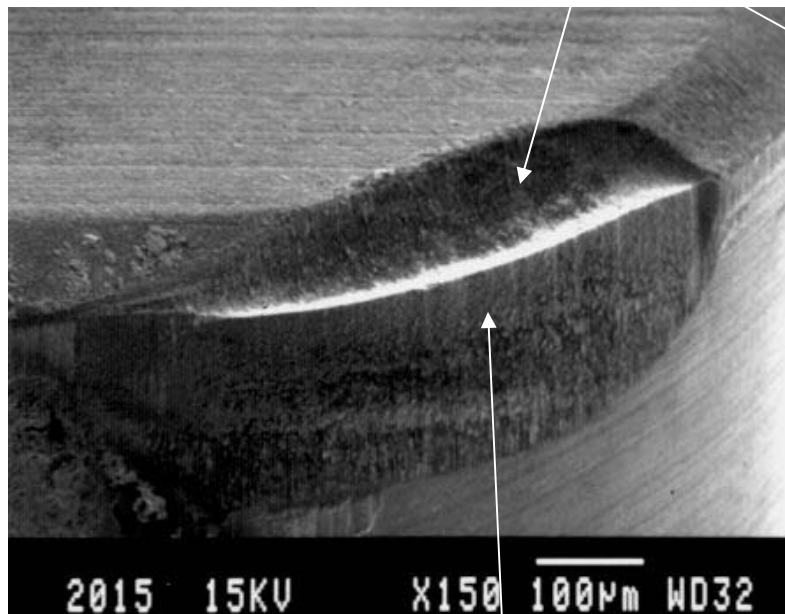
- Crater wear
- Flank wear
- Chipping: happens in aggressive cutting conditions
- Flank wear and crater wear are our interests in this study

### Main wear mechanisms in hard turning

- Abrasion: due to cementite and CBN particle (if have in high CBN tool) (Narutaki, *et al.*, 1979; Davies *et al.*, 1996)
- Adhesion: due to high temperature/stress along the tool/chip and tool/workpiece interfaces (Hooper, *et al.*, 1988; Chou, 1994; Davies *et al.*, 1996)
- Diffusion: binder material is not stable with iron due to high temperature (Narutaki, *et al.*, 1979; Konig, *et al.*, 1993)
- Tribochemical process: no convincing evidence yet
- Abrasion, adhesion, and diffusion are considered as basic mechanisms here

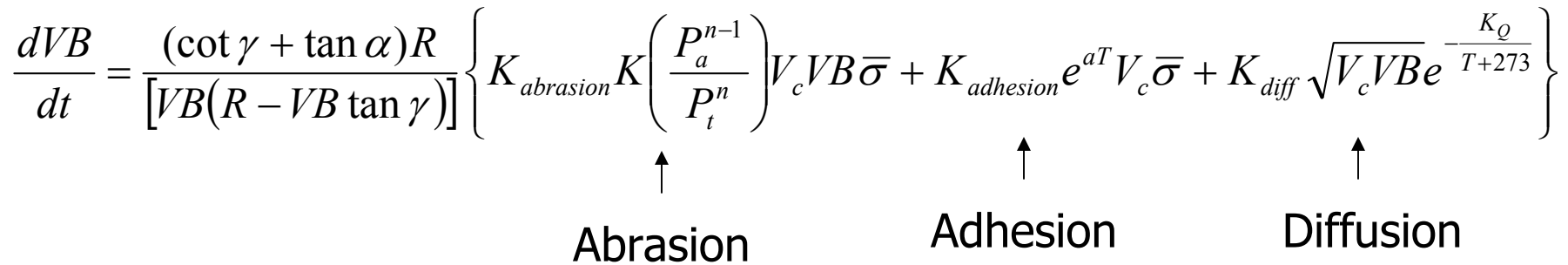
# Objective of this research

Crater wear



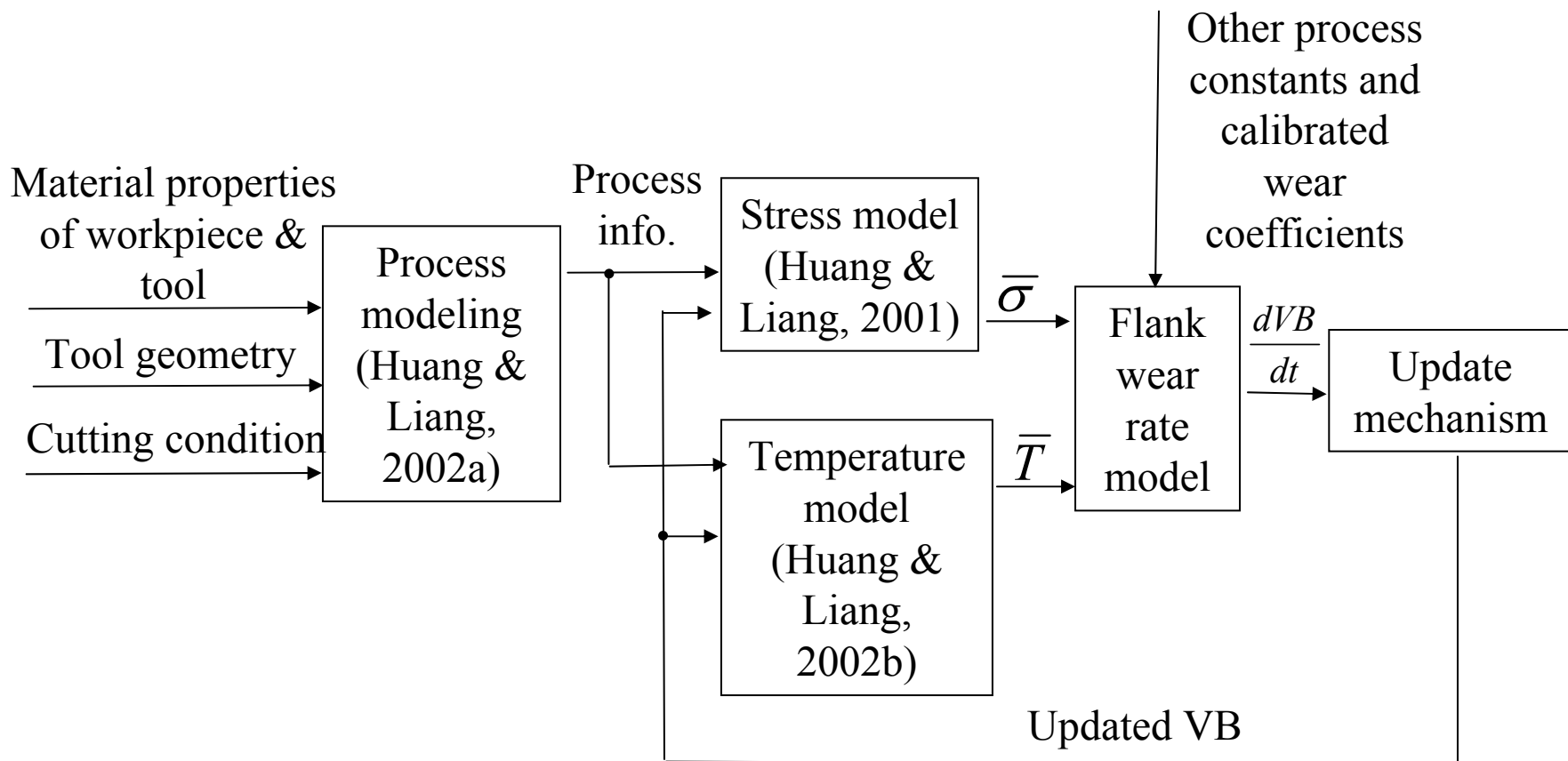
Flank wear

⇒ To develop a scientific, systematic, and reliable methodology to predict the tool flank/crater wear rates based on cutting condition and tool geometry for given tool and workpiece material properties.

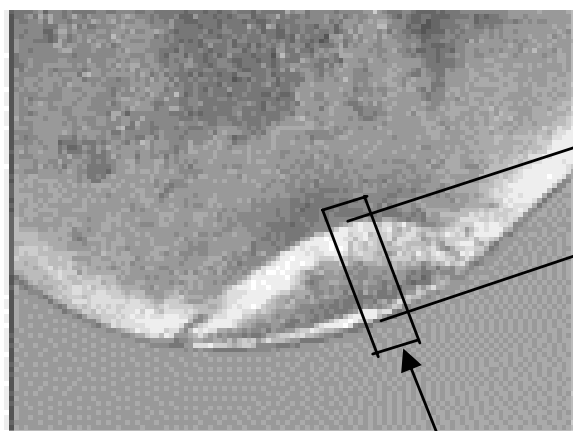




# Modeling of flank wear rate (cont'd)

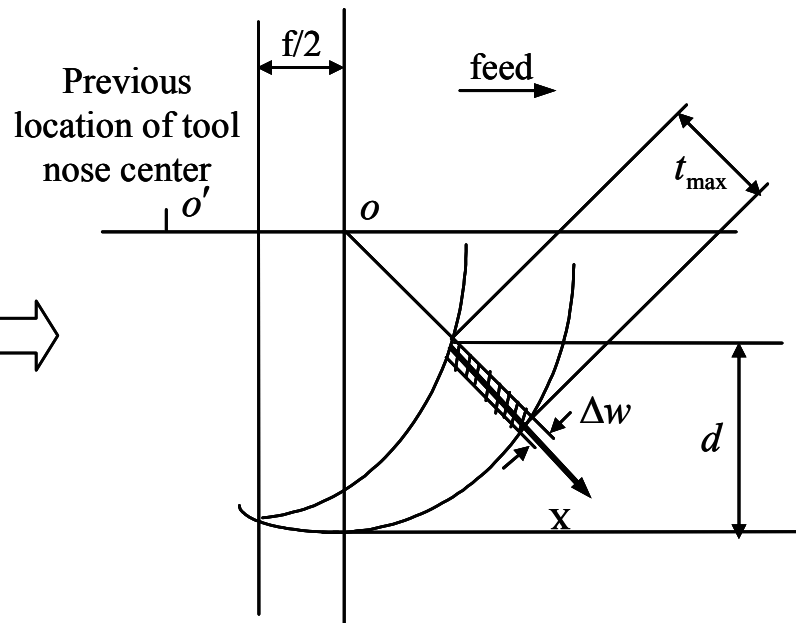


# Modeling of crater wear rate



Longest contact length due to  $t_{\max}$

Interested rectangular zone



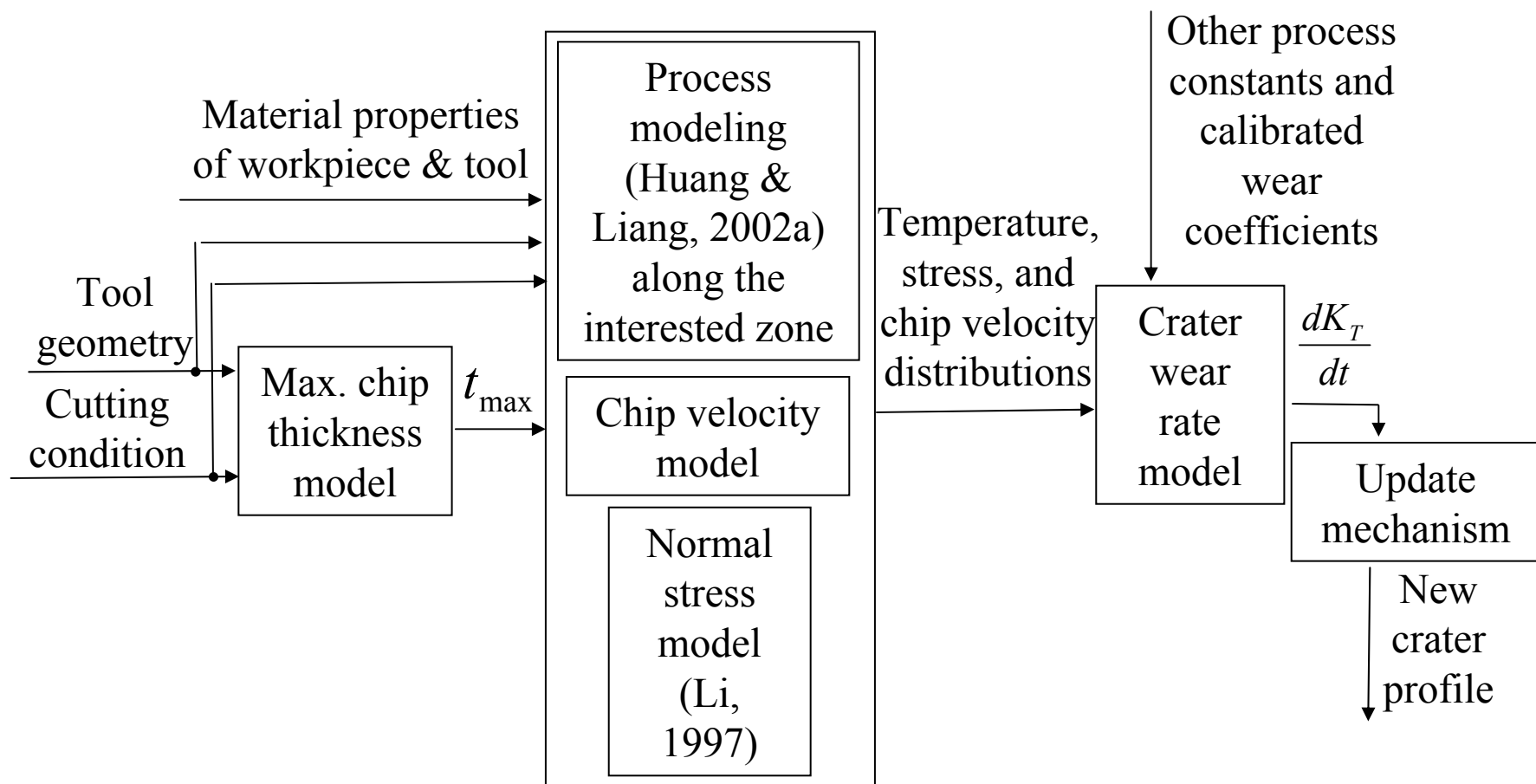
$$\frac{dK_T(x)}{dt} = K_{\text{abrasion}} K \left( \frac{P_a(x)^{n-1}}{P_t(x)^n} \right) V_{\text{chip}}(x) \sigma(x) + \frac{1}{h} K_{\text{adhesion}} e^{aT(x)} V_{\text{chip}}(x) \sigma(x) + K_{\text{diff}} e^{-\frac{K_Q}{T(x)+273}} \sqrt{V_{\text{chip}}(x)} \frac{(\sqrt{x+\Delta x} - \sqrt{x})}{\Delta x}$$

Abrasion

Adhesion

Diffusion

# Modeling of crater wear rate (cont'd)



# Calibration & validation of wear rate models

## ■ Calibration of wear rate model

$K_{abrasion}$ ,  $K_{adhesion}$ ,  $a$ ,  $K_{diff}$ ,  $K_Q$  need to be calibrated

Those coefficients depend on tool/workpiece combination.

## ■ Calibration steps

- Optimize the coefficients of wear rate model by minimizing the least square error between predicted and measured flank wear rates for three cutting conditions ( $v=1.520\text{m/s}$ ,  $f=.0760\text{mm/rev}$ ,  $doc=.203\text{mm}$ ;  $v=2.29\text{m/s}$ ,  $f=.168\text{mm/rev}$ ,  $doc=.203\text{mm}$ ;  $v=1.520\text{m/s}$ ,  $f=.0760\text{mm/rev}$ ,  $doc=.102\text{mm}$ ; ) (Huang and Liang, 2002c)

## ■ Validation steps

- Validate the flank wear rate model based on seven cutting conditions (Huang and Liang, 2002c)
- Validate the crater wear rate model based on three cutting conditions (Huang and Liang, 2002d)

# Calibrated wear rate models

- Tool material: Kennametal KD050
- Workpiece material: hardened 52100, 62HRC

$$\frac{dVB}{dt} = \frac{(\cot \gamma + \tan \alpha)R}{[VB(R - VB \tan \gamma)]}$$

$$\times \left\{ 0.0295K \left( \frac{P_a^{n-1}}{P_t^n} \right) V_c VB \bar{\sigma} + 1.4761 \times 10^{-14} e^{9.0313 \times 10^{-4} T} V_c \bar{\sigma} + 5.7204 \times 10^6 \sqrt{V_c VB} e^{-\frac{20460}{T+273}} \right\}$$

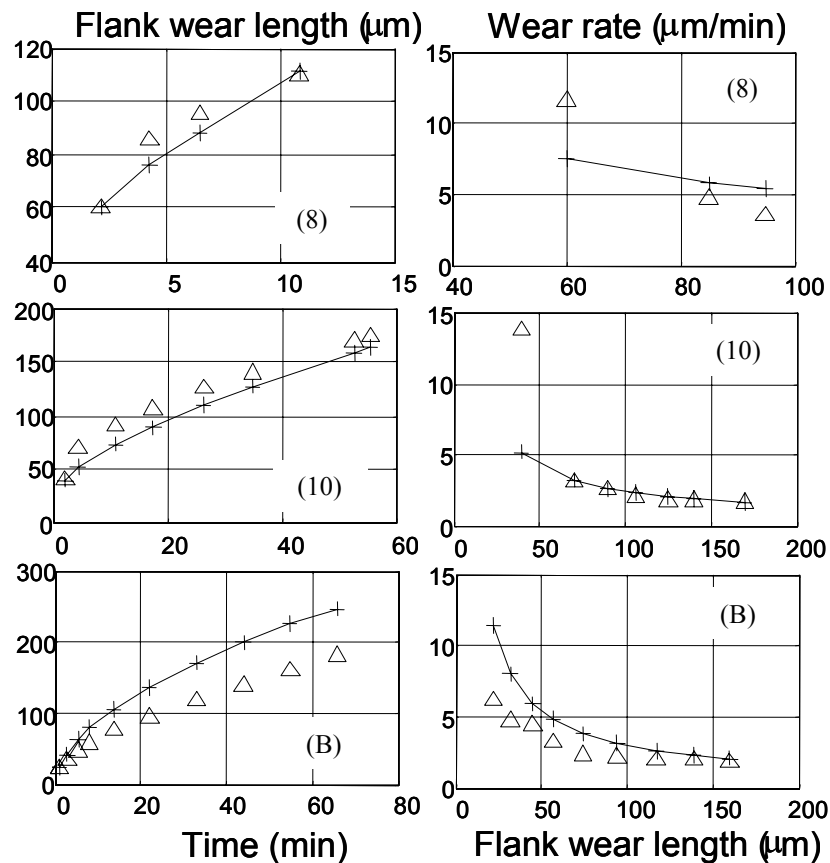
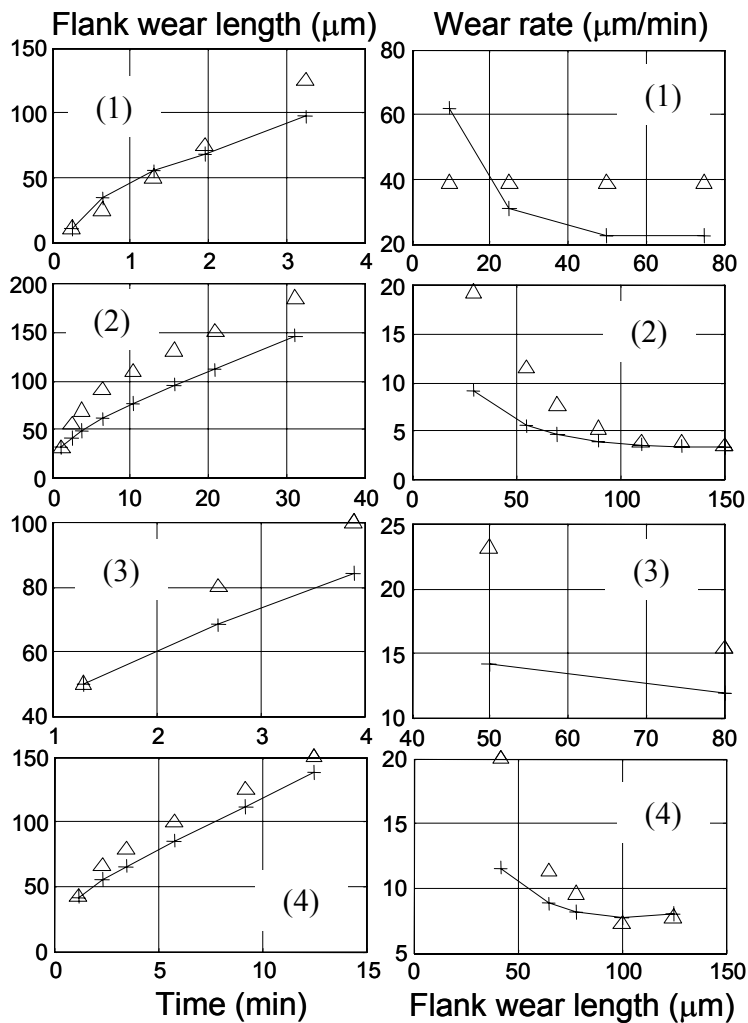
$$\frac{dK_T(x)}{dt} = 0.0295K \left( \frac{P_a(x)^{n-1}}{P_t(x)^n} \right) V_{chip}(x) \sigma(x)$$

$$+ 1.4761 \times 10^{-14} e^{9.0313 \times 10^{-4} T} \frac{1}{h} V_{chip}(x) \sigma(x)$$

$$+ 5.7204 \times 10^6 e^{-\frac{20460}{T+273}} \sqrt{V_{chip}(x)} \frac{(\sqrt{x + \Delta x} - \sqrt{x})}{\Delta x}$$

# Validation of flank wear rate model

## Flank wear progression

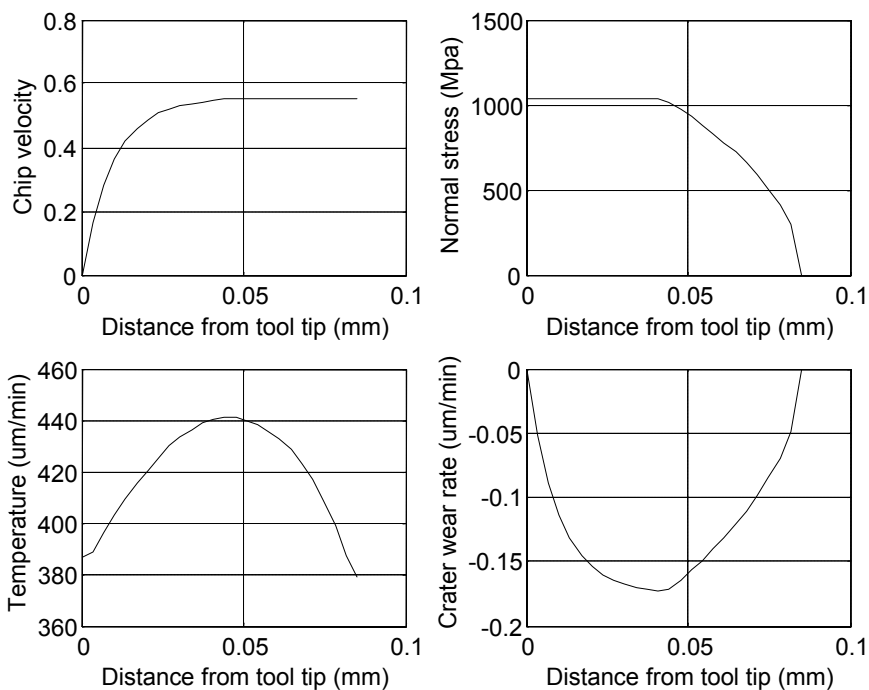


Solid line: predictions

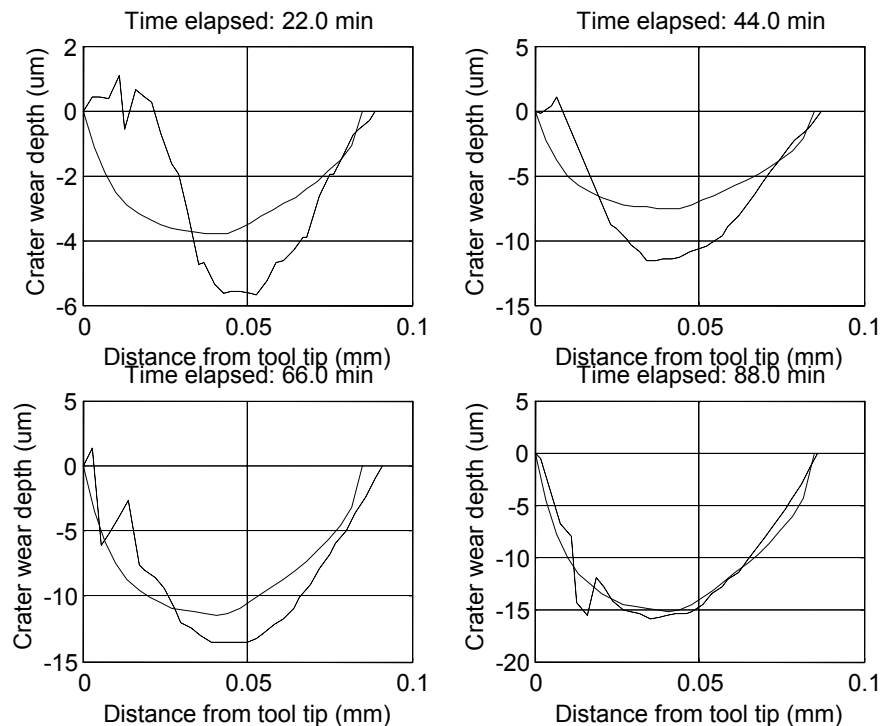
Triangular: measurements

# Validation of crater wear rate model

## Process information & crater wear rate



## Crater wear progression



Solid line: predictions; dash line: measurements

Cutting conditions:

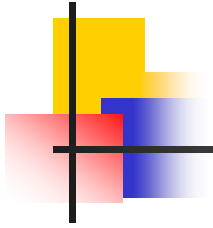
cutting speed: 1.52 m/s, feedrate: 0.076 mm/rev, depth of cut: 0.102 mm

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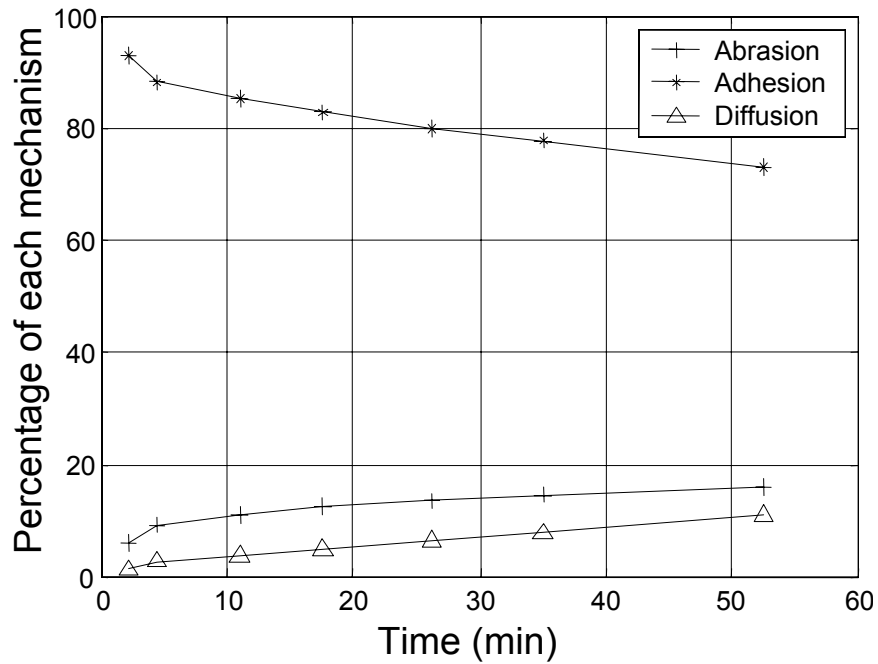
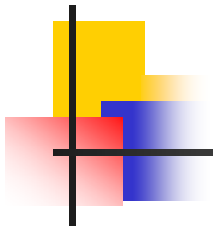
## Summary:

- Abrasion, adhesion, and diffusion in hard turning are considered as the main wear mechanisms for the progressive tool wear. The total tool wear rate is contributed from abrasion, adhesion, and diffusion mechanisms.
- The progressive tool flank/crater wear can be modeled as the function of cutting condition and tool geometry for a given tool/workpiece combination in a reasonable accuracy in hard turning.

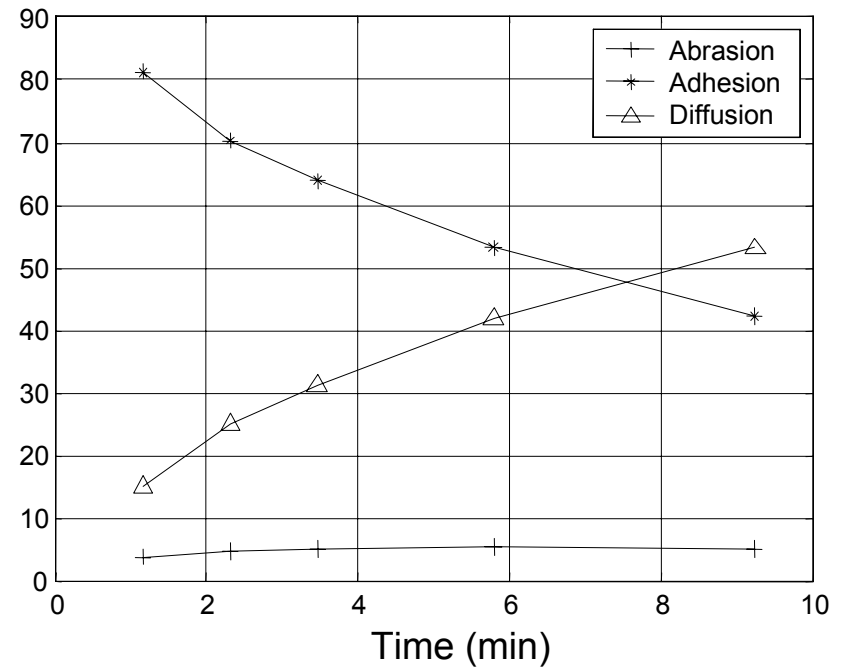




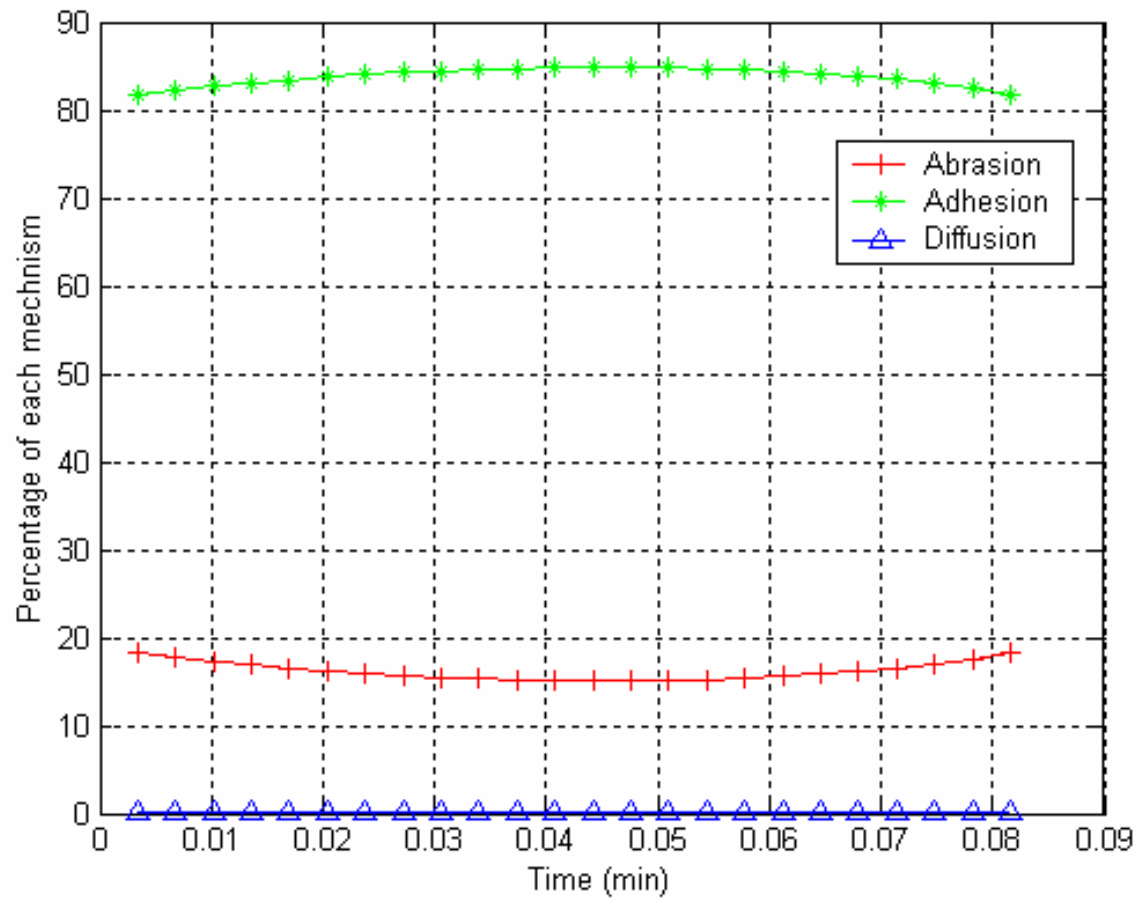
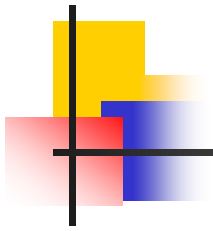
# Questions?



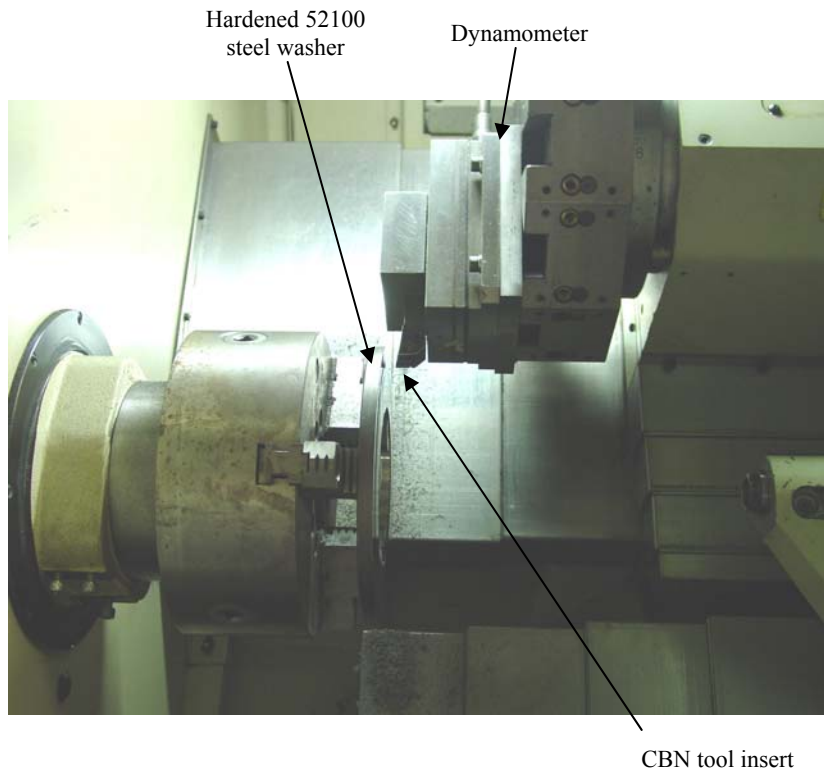
General cutting condition (#10)



Aggressive cutting condition (#4)



## Pin-on-disk



Goal: to identify the wear coefficients under semi-sliding conditions without the effect of diffusion wear.